© Universiti Tun Hussein Onn Malaysia Publisher's Office





Journal of Advancement in Environmental Solution and Resource Recovery

http://publisher.uthm.edu.my/ojs/index.php/jaesrr

e-ISSN : 2821-2819

# A Laboratory Investigation on Flow Rate Coefficient for Compound Weir

# Nur Aina Atirah Othman<sup>1</sup>, Zarina Md Ali<sup>1\*</sup>, Noor Aliza Ahmad<sup>1</sup>

<sup>1</sup>Department of Civil Engineering, Faculty of Civil Engineering and Built Environment, Universiti Tun Hussein Onn Malaysia, Batu Pahat, 86400, MALAYSIA

\*Corresponding author

DOI: https://doi.org/10.30880/jaesrr.2022.02.02.012 Received 14 August 2022; Accepted 18 December 2022; Available online 28 December 2022

Abstract: The application of the weir can be used to determine the flowrate in an open channel. Thus, the coefficient of flow rate is an important consideration when using weirs because its value is dependent on the shape of the weir. Compound weirs are an appropriate structure for rivers with low flow levels during the dry season and high flow levels during the rainy season. The objective of the study is to determine the flowrate coefficient,  $C_d$  using a combination of rectangular-triangular (V-notch) shape weir. An experimental study using nine models of compound weirs with different measurements of V-notch angle,  $\theta$  (30°, 50°, and 80°) and width of rectangular weir, L (0.1 m, 0.12 m and 0.15 m). Result shows the highest and lowest value for  $C_d$  is 0.47 (Model 2 at water level, H = 0.076 m) and 0.11 (Model 8 at water level, H = 0.025 m, respectively. The most efficient combination is a compound weir with a V-notch angle of = 500 and a rectangular shape width of L = 0.1 m. The correlation between  $C_d$  and H, and  $Q_{exp}$  and  $Q_{theory}$  shows good relationship between variables, except for Model 7. It is show that the flowrate and characteristics of the weir influence the flowrate coefficient,  $C_d$ . In conclusion, the value of the flow rate coefficient, Cd, can be determined for both high and low water flows prior to its application on the actual site. The hydraulic structure must therefore conform to a precise discharge value as a design criterion. If the discharge is overestimated, the structure may collapse, and if it is underestimated, the structure may not last long due to its inherent fragility.

Keywords: Compound weirs, flowrate coefficient, experimental study, rectangular-triangular weir

# 1. Introduction

Weirs are structures that form a barrier across the width of a river, altering the flow characteristics and usually resulting in a change in river level, as well as allowing flow rates to be measured as a function of depth. The most common shapes for weirs are rectangular, trapezoidal, and triangular (V-notch); however, each of these shapes has drawbacks and is not ideal in all situations [1]. Among these shapes, the V-notch has an easy structure and can accurately measure flow in a natural or manmade channel.

Compound weirs are made up of various types of weirs. Compound sharp-crested weirs are becoming more popular due to their simplicity, ease of maintenance, and high flow measurement precision. However, compound weirs are appropriate for dams with low flow levels during the dry season and high flow levels during the rainy season. A compound weir may be an appropriate solution in situations where flow rates are expected to vary greatly [2][3]. The V-notch is made for situations with low flow, while the rectangular weir is used to measure flows that are higher. The designed hydraulic structure must fulfil the design requirement, which is an accurate value of discharge. If the discharge is overestimated, the structure may fail; if the discharge is underestimated, the structure may fail due to weakness. [4].

Numerous laboratory studies on compound weirs have been conducted to determine performance using rectangular and triangular weir shapes or combinations of these shapes [5–15]. The models of sharp-crested weirs were mostly used

in the experiments. According to the findings of their research, the flow characteristics and geometry of the weir and channel influence the flowrate coefficient.

Therefore, experimental study is needed to determine coefficient of the flowrate,  $C_d$ , of compound weirs with different sizes of openings. This allows for accurate observations of streams with a wide variety of flow rates. The objectives of this study are to determine the coefficient of flow rate,  $C_d$  of compound weirs (rectangular – triangular) and to correlate the relationship between the  $Q_{theory}$  and  $Q_{exp}$  and between coefficient of flow rate,  $C_d$ , and height of water, H. Compound weirs were created by combining rectangular and triangular (V-notch) cut-outs. This study can be used to determine the value of Cd for high and low water flows before it is used at the site. It is possible to manage the water flow of the drainage system by determining the necessary coefficient of flow rate,  $C_d$ . This raises the water level, allowing water to be redirected by the canal to the agricultural field due to the difference in head.

### 2. Materials and Methods

Multiple experiments on the compound (rectangular-triangular) weir were conducted at the Fluid Laboratory, Faculty of Civil Engineering and Built Environment. The equipment and experimental procedures are discussed further below.

# 2.1 Experimental Equipment

The compound weir (Fig. 1) was created in nine thin plate models with specific measurements. Table 1 displays the dimensions of weir models with various V-notch angles,  $\theta$  (30°, 50°, and 80°) and rectangular widths, L. (0.10 m, 0.12 m, and 0.15 m). The constant values for these models are: (1) length of the weir, B is 0.25 m, (2) height of the weir from the datum, P is 0.06 m, (3) height of the weir sample, 0.16 m, and (4) thickness of the weir plate, 3 mm.

The hydraulic bench (Fig. 2) serves as a short-distance channel, complete with a small water tank and a pump that rechannels water through a pipe and back into the water tank. The outlet in the reservoir base is linked to a piezometer, which is used with a timer to measure the flow rate.



Fig. 1 - Sketch of compound (rectangulartriangular) weir



Fig. 2 - Hydraulic bench

#### Table 1 - Dimensions of the weir model

Model	1	2	3	4	5	6	7	8	9
Triangular angle, θ	30	50	80	30	50	80	30	50	80
Rectangular Width, L (m)	0.10	0.10	0.10	0.12	0.12	0.12	0.15	0.15	0.15

#### 2.2 Experimental Procedures

The laboratory safety procedure was identified and followed before, during, and after the experiment. After that, the equipment must be inspected to ensure that it is in good working order. The experiments were carried out using nine different measurement of weir plates, with the height of the water and the duration of the flow being recorded. The procedure for this experiment is as follows: A weir model was placed on a hydraulic bench, and the gap between the weir model and the hydraulic bench was filled with plasticine. The control valve was then adjusted for the highest level of water in the tank. The data measured involved the height of water,  $H_1$  and  $H_2$ , time to flow, T, at a volume of 3 liters (collected in the volumetric tank). These steps were carried out several times by increasing the control valve to increase the water level for each compound weir model.

#### 2.3 Equations

The Bernoulli equation is commonly used to solve the force and energy problem that is frequently encountered in engineering practise, and it provides the theoretical foundation for solving hydraulic calculations in actual engineering [16]. These equations were applied and were very significant in this study. The related equations are;

i. Experimental flow rate, Q<sub>exp</sub>

$$Q_{exp} = V/t \tag{1}$$

where, V = volume = 3 Liters and t = time (s)

ii. Theoretical flow rate

$$Q_{\text{theory}} = \frac{8}{15} C_d \sqrt{(2g)} \tan \frac{\theta}{2} H_1^{\frac{3}{2}} + \frac{2}{3} C_d \sqrt{2g} L H_2^{\frac{3}{2}}$$
(2)

Where,  $C_d$  = coefficient of flow rate, g = gravitational acceleration,  $H_1$  = the height of water in V-notch,  $H_2$  = the height of water in rectangular weir,  $\theta$  = V- shape angle, L = width of rectangular weir

Then, the coefficient of flow rate,  $C_d$  is the ratio of the actual flow rate that goes through the gauge compared to the theoretical flow rate. The equation can be written as:

$$C_{d} = \frac{\text{Actual flow}}{\text{Theoretical flow}}$$
$$C_{d} = \frac{Q_{exp}}{Q_{theory}}$$
(3)

R-squared and linear regression are useful in determining the strength of a relationship between two variables, allowing one value to be predicted in a model. Almost all studies involving the strength of the relationship between variables and other variables employ this statistical technique [17].

#### 3. Results and Discussion

The experiments were carried out for 14 to 16 trials to collect data on nine different weir models, which are summarized in Table 2. The results show that the minimum and maximum water heights that can be recorded are 0.025 m (Model 7 and 8) and 0.079 m (Model 1), respectively. While the average of water height ranged between 0.049 m and 0.058 m. When comparing all models, the height of the water decreases as the V-notch angle and rectangular length of the weir increase, for example, the maximum level for model 3 is 0.005 m lower than Model 2, but still higher than Model 6.

Model		1	2	3	4	5	6	7	8	9
Height of	Min	0.029	0.027	0.026	0.028	0.026	0.028	0.025	0.025	0.025
water, H =	Max	0.079	0.076	0.071	0.078	0.075	0.068	0.077	0.070	0.066
$H_1 + H_2(m)$	Ave	0.057	0.056	0.051	0.057	0.053	0.050	0.058	0.053	0.049
0 ( 10 ]	Min	0.025	0.028	0.038	0.023	0.021	0.038	0.012	0.012	0.051
$Q_{exp} (x \ 10^{-3} m^{3/s})$	Max	0.691	0.862	0.779	0.767	0.763	0.826	0.783	0.804	0.872
111 73)	Ave	0. 283	0.347	0.368	0.294	0.313	0.355	0.309	0.325	0.395
0 ( 10 3	Min	0. 091	0.132	0.216	0.083	0.120	0.216	0.063	0.109	0.196
$Q_{\text{theory}}$ (x 10 <sup>-5</sup> m <sup>3</sup> /s)	Max	1.812	1.854	2.007	1.896	2.017	1.964	2.319	1.869	2.005
111 73)	Ave	0.760	0.926	1.114	0.802	0.875	1.036	1.034	0.950	1.082
	Min	0.27	0.21	0.18	0.28	0.18	0.18	0.19	0.11	0.26
$C_d$	Max	0.4	0.47	0.41	0.41	0.41	0.42	0.35	0.43	0.44
	Ave	0.35	0.34	0.29	0.34	0.32	0.30	0.28	0.29	0.34

Table 2 - Experimental results for compound weirs

Furthermore, the  $Q_{exp}$  and  $Q_{theory}$  varied from 0.283 x 10<sup>-3</sup> m<sup>3</sup>/s to 0.395 x 10<sup>-3</sup> m<sup>3</sup>/s, and from 0.76 x 10<sup>-3</sup> m<sup>3</sup>/s to 1.114 x 10<sup>-3</sup> m<sup>3</sup>/s, respectively. The calculated minimum and maximum value for  $Q_{theory}$  are 0.063 x 10<sup>-3</sup> m<sup>3</sup>/s and 2.017 x 10<sup>-3</sup> m<sup>3</sup>/s, respectively, while the minimum and maximum values recorded by  $Q_{exp}$  are 0.012 x 10<sup>-3</sup> m<sup>3</sup>/s and 0.862 x 10<sup>-3</sup> m<sup>3</sup>/s, respectively, both of which are less than  $Q_{theory}$ .

## 3.1 Coefficient of Flow Rate, Cd

According to Table 2, the minimum and maximum values for the flow rate coefficient,  $C_d$ , are 0.11 (Model 8) and 0.47 (Model 2), respectively, while the average value ranged from 0.28 to 0.35. As a result, Model 1 has the best optimum value of  $C_d$  0.35. Apart from Models 7-9, the average  $C_d$  decreases as the V-notch angles increase, while the width of the rectangular weir, L, remains constant.

The distribution of Cd is shown in Fig. 3 based on the number of experiment trials performed on nine compound weir models. At the maximum water heights of the experiment trials, the C<sub>d</sub> ranged between 0.34 and 0.47, with Model 7 recording the lowest value at H = 0.077 m. The best value of C<sub>d</sub> for L = 0.10 m and 0.15 m is 0.47 and 0.44, respectively at  $\theta = 50^{\circ}$ . While for L = 0.12 m, the best value of C<sub>d</sub> is 0.42 at  $\theta = 80^{\circ}$ .



Fig. 3 - Distribution of coefficient of flowrate, Cd

#### 3.2 Relationship Between Coefficient of Flow Rate, Cd and Height of Water, H

Figure 4 depicts the relationship between  $C_d$  and water height, H, where the value of  $C_d$  varies across all models. Model 7 has the weakest relationship with 0.29, which has large value fluctuations in Fig. 4. (c). Meanwhile, Table 3 shows the  $R^2$  value of the linear equation Y = mX + c, where  $Y = C_d$  and X = H.

The results show that the V-notch angle,  $\theta = 30^{\circ}$ , has a moderate relationship with Models 1 and 4, however a poor correlation with Model 7. For V-notch angle,  $\theta = 50^{\circ}$ , both variables exhibit a strong relationship with  $R^2 \ge 0.9$  at Models 2, 5, and 8. Lastly, for V-notch angle,  $\theta = 80^{\circ}$ , there is a good relationship with  $R^2 \ge 0.94$  at Models 3 and 6, but moderate correlation at Model 9. This demonstrates that the V-notch angle,  $\theta = 50^{\circ}$ , is the best angle of V-notch when compared to rectangular weir widths, L (0.1 m, 0.12 m, and 0.15 m). Therefore, Model 3 is the best model in terms of variable correlation, while Model 6 has the highest increment among models, with m = 5.98. In conclusion,  $R^2 > 0.9$  indicates that Models 2, 3, 5, 6, and 8 have a good relationship between C<sub>d</sub> and H.



Fig. 4 - Relationship between coefficient of flow rate, C<sub>d</sub> and height of water, H according to compound weir models

Model	1	2	3	4	5	6	7	8	9
Equation,	V-2 22-	V-4 57.	V-5.26.	V-2.24.	V=4.00m	V-5.08-	V-1 75.	V-5.05w	V-4.25
Y=mX + c	+0.2245	+0.0801	+0.0239	+0.2054	+0.1064	+0.0031	+0.1758	+0.0279	+0.1223

Table 3 - Derived equation between Cd and H

$\mathbb{R}^2$	0.78	0.94	0.96	0.72	0.93	0.94	0.29	0.9	0.76
*where V =	= Cd and $X = I$	Н							

According to Fig. 5, all models show that as H increases, so does the value of Cd, even though Model 7 recorded some data that is far from the average value. All models, except Model 7 ( $C_d = 0.34$ ) achieved  $C_d \ge 0.4$  at H = 0.07 m, while at H = 0.03 m, all models achieved  $C_d = 0.23 \pm 0.03$  except Model 3. Most of the value of  $C_d$  is scattered between 0.2 and 0.4, however when H  $\ge 0.06$  m, the value of  $C_d$  begins to increase more than 0.4. As the study was carried out in a short-distance channel with a height of less than 0.17 m, the value of  $C_d$  cannot be recorded at more than 0.47 as there is insufficient channel height to raise the water level in the channel. Using the equation in Table 3,  $C_d$  can be determined for any value of H, for example, if H = 0.1 m, value of  $C_d = 0.55$  using Y = 5.26x +0.0239 (equation Model 3).



Fig. 5 - Distribution of coefficient of flow rate, Cd versus height of water, H

#### 3.3 Relationship Between the Qtheory and Qexp

Based on the width of the rectangular weir, L, Fig. 6 depicts the relationship between theoretical flow rate,  $Q_{theory}$ , and experimental flow rate,  $Q_{exp}$ . Figure 5 (a) shows that the V- shape angles,  $\theta = 50^{\circ}$  and  $\theta = 30^{\circ}$  had the highest and lowest values of  $Q_{exp}$ , with 0.000862 m<sup>3</sup>/s and 0.000691 m<sup>3</sup>/s, respectively. Meanwhile, the highest and lowest values of  $Q_{theory}$  are at  $\theta = 80^{\circ}$  and  $\theta = 30^{\circ}$ , respectively, with values of 0.002007 m<sup>3</sup>/s and 0.001812 m<sup>3</sup>/s. According to Figure 5 (b), V-notch, = 80^{\circ} had the highest  $Q_{exp}$ , with a value of 0.000826 m<sup>3</sup>/s, and = 50^{\circ} had the lowest, with 0.000763 m<sup>3</sup>/s. In contrast, the highest and lowest of  $Q_{theory}$  were obtained by  $\theta = 50^{\circ}$  and  $\theta = 30^{\circ}$  with values of 0.002017 m<sup>3</sup>/s and 0.001896 m<sup>3</sup>/s, respectively.

Furthermore, graphs in Figure 5 (c) show that the highest and lowest  $Q_{exp}$  values were at = 80° (0.000872 m<sup>3</sup>/s) and = 30° (0.000783 m<sup>3</sup>/s), respectively. Meanwhile, the highest and lowest values of  $Q_{theory}$  are at = 30° and 50°, respectively, with values of 0.002319 m<sup>3</sup>/s and 0.001869 m<sup>3</sup>/s.

These graphs depict the direct proportional between  $Q_{theory}$  and  $Q_{exp}$ , with  $Q_{theory}$  always being greater than  $Q_{exp}$ . As a result, as the  $Q_{exp}$  increases, so will the  $Q_{theory}$ . Nevertheless, Model 7 demonstrates a fluctuating relationship between these variables. Therefore, a comparison between  $Q_{exp}$  and  $Q_{theory}$  is required to validate the value of the coefficient of flow rate, Cd, for estimating the flow rate at the field site.



Fig. 6 - Comparison between Qexp and Qtheory for nine models

Table 4 displays the linear equation Y = mX + c, as well as the R-squared (R<sup>2</sup>) value. Y = mX + c equation was used in conjunction with the expressions  $Y = Q_{exp}$  and  $X = Q_{theory}$ . All the models have positive values for the gradient m, between 0.39 and 0.46, and the R<sup>2</sup> values ranged from 0.96 to 1.00. This demonstrates the strength of the relationship that exists between the two variables.

Model 1 2 9 3 4 5 6 7 8 Y=0.39x Y=0.46x Y=0.44x Y=0.41x Y=0.41x Y=0.44x Y=0.33x Y=0.41x Y=0.46x Y=mX+c-1x10<sup>-05</sup> -1x10<sup>-5</sup> -8x10<sup>-5</sup> -4x10<sup>-5</sup> -4x10-5 -1x10-4 -6x10<sup>-5</sup> -1x10<sup>-4</sup> -3x10<sup>-5</sup>

0.99

Table 4 - Equation from relationship of  $Q_{exp}$  and  $Q_{theory}$ , and R-squared

1.00

0.97

0.96

0.98

0.96

#### 4. Conclusion

1.00

0.98

0.97

 $\mathbb{R}^2$ 

In conclusion, study on nine compound weir models reveals that the width of the rectangular weir, L, and the Vnotch angle, influence the value of  $C_d$ . The highest value for  $C_d$  is 0.47 which characteristics weir, L = 0.10 m,  $\theta = 50^{\circ}$ (Model 2) at H = 0.076 m. Meanwhile, the lowest value of  $C_d$  is 0.11 which characteristics weir, L = 0.15 m,  $\theta = 50^{\circ}$ (Model 8) at H = 0.025 m. However, this study was unable to achieve  $Cd \ge 0.47$  because the experiments could not raise the water level higher than 0.08 m, thus the equation between  $C_d$  and H can be used to estimate value of  $C_d$  by given H. Furthermore, when compared to all model results, the most effective combination of V-notch angle, = 50°, and rectangular shape width, L = 0.1 m. Except for Model 7, the correlation between Cd and H, and  $Q_{exp}$  and  $Q_{theory}$ , shows good relationships between variables. Before being used at the actual site, the value of  $C_d$  can be determined using this study for high and low water flows. It is possible to manage the drainage system's water flow or raise the water level, allowing water to be redirected by the canal to the agricultural field due to the difference in head, by determining the necessary flowrate coefficient,  $C_d$ . The installation of a compound weir in the dam will improve water flow control. Furthermore, this study can be used as a guide and reference point for future researchers studying the flowrate coefficient of rectangular-triangular weirs.

#### Acknowledgement

The authors would like to thank the Faculty of Civil Engineering and Built Environment, Universiti Tun Hussein Onn Malaysia for supporting this study.

#### References

- Irzooki, R. H., Akib, S. M., & Fayyadh, M. M. (2014). Experimental Study of Characteristics of Flow over Weirs with Semicircular Openings. *Arabian Journal for Science and Engineering*, 39(11), 7599–7608. https://doi.org/10.1007/s13369-014-1360-8
- Ali, A. A. M., Ibrahim, M., & Diwedar, A. I. (2015). The Discharge Coefficient for a Compound Sharp Crested V-Notch Weir. Asian Journal of Engineering and Technology, 3(5).
- Zakwan, M. & Khan, I. (2020). Estimation of Discharge coefficient for side weirs. *Water and Energy International* 62(11):71-74.
- Kumar, S., Ahmad, Z. & Mansoor, T. (2011). A new approach to improve the discharging capacity of sharp-crested triangular plan form weirs. *Flow Measurement and Instrumentation*, 22(3), 175–180.
- Alhamid, A. A., Negm, A. Z. & Albrahim, A. M. (1997). Discharge equation for proposed self-cleaning device. Journal of King Saud University - Engineering Sciences, 9(1), pp. 13-24.
- Abozeid, G., Mohamed, H. I., and Shehata, S., M. (2010). Hydraulics of clear overfall weirs with bottom-openings. Ain Shams Engineering Journal, 1(2), pp. 115-119.
- Ameri, M., Ahmadi, A. & Dehghani, A. A. (2015). Discharge coefficient of compound triangular-rectangular sharpcrested side weirs in subcritical flow conditions. *Flow Measurement and Instrumentation*, 45, pp. 170–175.
- Ansari, M. A., Hussain, A., Shariq, A. & Alam, F. (2019). Experimental and numerical studies for estimating coefficient of discharge of side compound weir. *Canadian Journal of Civil Engineering*, 46(10), pp. 887-95.
- Alwan, H. H, Saleh, L. A. M., Al-Mohammed, F. M. & Abdulredha, M. A. (2020). Experimental Prediction of The Discharge Coefficients for Rectangular Weir with Bottom Orifices. *Journal Of Engineering Science and Technology*, 15(5), pp. 3265 – 3280.
- Piratheepan, M., Winston, N. E. F. & Pathirana, K. P. P. (2007). Discharge Measurements in Open Channels using Compound Sharp-Crested Weirs. Engineer: Journal of the Institution of Engineers, Sri Lanka, 40(3), pp. 31-38.

- Bagheri, S., Kabiri-Samani, A. R. & Heidarpour, M. (2014). Discharge coefficient of rectangular sharp-crested side weirs Part II: Domínguez's method. *Flow Measurement and Instrumentation*, 35, pp. 116–121.
- Ibrahim, M., Sayed D. A., Azim, A., Ali, M., Ibrahim, M. & Diwedar, A. I. (2015). The Discharge Coefficient for a Compound Sharp Crested V-Notch Weir. In *Asian Journal of Engineering and Technology*, 3(5), pp. 494-501
- Kulkarni, K. H. & Hinge, G. A. (2020). Experimental Study for Measuring Discharge Through Compound Broad Crested Weir. *Flow Measurement and Instrumentation*, 75(2):101803, pp. 1-18.
- Zahiri, A., Azamathulla, H. M. & Bagheri, S. (2013). Discharge coefficient for compound sharp crested side weirs in subcritical flow conditions. *Journal of Hydrology*, 480, pp. 162–166.
- Ibrahim, M. M. (2015). Bed profile downstream compound sharp crested V-notch weir. *Alexandria Engineering Journal*, 54(3), pp. 607-613.
- Qin, R., & Duan, C. (2017). The principle and applications of Bernoulli equation. *Journal of Physics: Conference Series*, 916(1), pp. 1-6.
- Kilic, S. (2013). Linear Regression Analysis. Journal of Mood Disorders, 3(2), pp. 90-93.